







THS3091, THS3095

SLOS423K - SEPTEMBER 2003 - REVISED APRIL 2023

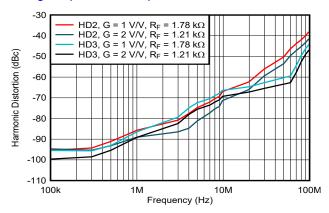
# THS309x High-Voltage, Low-Distortion, Current-Feedback Operational Amplifiers

#### 1 Features

- Low distortion:
  - 84-dBc HD2 at 10 MHz,  $R_1 = 1 \text{ k}\Omega$
  - 99-dBc HD3 at 10 MHz,  $R_I = 1 \text{ k}\Omega$
- Low noise:
  - 15-pA/√Hz noninverting current noise
  - 14-pA/√Hz inverting current noise
  - 1.1-nV/√Hz voltage noise
- High slew rate:  $6000 \text{ V/}\mu\text{s}$  (G = 5,  $V_O$  = 20  $V_{PP}$ )
- Wide bandwidth: 305 MHz (G = 2,  $R_1$  = 100  $\Omega$ )
- High output current drive: ±310 mA
- Wide supply range: ±5 V to ±16 V
- Power-down feature: THS3095 only

# 2 Applications

- High-voltage arbitrary waveform generators
- Pin Driver
- Power-FET drivers
- Source measurement unit (SMU)
- High capacitive load piezo element drivers



HD2 and HD3 vs Frequency at  $R_L = 100 \Omega$ 

#### 3 Description

The THS3091 and THS3095 (THS309x) are highvoltage, low-distortion, high-speed, current-feedback amplifiers that operate over a wide supply range of ±5 V to ±16 V. These devices are an excellent choice for applications that require large, linear output signals, such as pin drivers, power-FET drivers, and arbitrary waveform generators.

The THS3095 features a power-down pin (PD) that puts the amplifier into a low-power standby mode, and lowers the guiescent current from 9.5 mA to 500 µA.

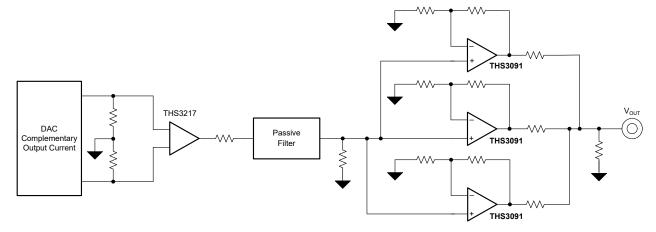
The wide, 32-V supply range, 6000-V/µs slewrate, and 310-mA output current drive make the THS309x an excellent choice for high-voltage arbitrary-waveform-driver applications. Moreover, with the ability to handle large voltage swings driving into low-resistance and high-capacitance loads while maintaining good settling time performance, these devices are an excellent choice for pin-driver and power-FET driver applications.

The THS309x are offered in an 8-pin SOIC (DDA) PowerPAD™ integrated circuit package. The THS3091 is also offered in an 8-pin HVSSOP (DGN) package.

#### Device Information(1)(2)

PART NUMBER	PD PIN PACKAGE			
THS3091	No	DDA (SO PowerPAD, 8)		
TH53091		DGN (HVSSOP, 8)		
THS3095	Yes	DDA (SO PowerPAD, 8)		

- For all available packages, see the orderable addendum at (1)the end of the data sheet.
- (2)For more information, see the *Device Comparison Table*.



Typical Arbitrary Waveform Generator Output Drive Circuit



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•	Removed specified operating voltage specifications from <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and $I_S = \pm 15 \text{ V}$ and $I_S$	
	Characteristics: $V_S = \pm 5 V$ tables	
•	Updated power supply rejection specifications in <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S = \pm 15 \text{ V}$ and <i>Electrical Characteristics:</i> $V_S $	
_	Characteristics: V <sub>S</sub> = ±5 V tables	
•	Changed Electrical Characteristics THS3095 to <i>Electrical Characteristics:</i> $V_S = \pm 5V$	
	Removed Dissipation Ratings table	
•	Updated Typical Characteristics (±5 V) section	
	Updated Feature Description section	
	Updated Device Functional Modes section	
•	Updated Application and Implementation section.	
•	Updated Typical Application section.	
•	Updated Layout section	
_	<u> </u>	
CI	hanges from Revision H (October 2015) to Revision I (December 2022)	Page
•	Updated the numbering format for tables, figures, and cross-references throughout the document	
•	Added the DGN package information to the data sheet	
•	Added the Device Comparison Table section	
•	Updated Thermal Information table	5



# **5 Device Comparison Table**

DEVICE	MAX SUPPLY, V <sub>S</sub> (V)	SSBW, A <sub>V</sub> = 5 (MHz)	MAXIMUM ICC AT 25°C (mA)	INPUT NOISE V <sub>n</sub> (nV/√Hz)	SLEW RATE (V/µs)	LINEAR OUTPUT CURRENT (mA)
THS3491	±16	900	17.3	1.7	8000	±420
THS3095	±16	205	10.5	1.1	6000	±310
OPA695	±6	700 (A <sub>V</sub> = 4)	13.3	1.8	4300	±90
THS3001	±16	350	7.5	1.6	6300	±120
THS3115	±15	100 (A <sub>V</sub> = 4)	5.5	2.2	1550	±270

# **6 Pin Configuration and Functions**

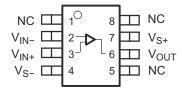


Figure 6-1. DGN or DDA Package, 8-Pin SOIC, HVSSOP or SO-PowerPAD THS3091 (Top View)

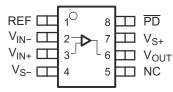


Figure 6-2. DDA Package, SO-PowerPAD THS3095 (Top View)

**Table 6-1. Pin Functions** 

	PIN						
NAME	N	0.	TYPE <sup>(1)</sup>	DESCRIPTION			
NAME	THS3091	THS3095					
NC	1, 5, 8	5	_	No connection			
PD	_	8	I	mplifier power down ow = amplifier disabled ligh (default) = amplifier enabled			
REF	_	1	I	Voltage reference input to set PD threshold level			
V <sub>IN</sub> _	2	2	I	Inverting input			
V <sub>IN+</sub>	3	3	I	Noninverting input			
V <sub>OUT</sub>	6	6	0	Output of amplifier			
V <sub>S-</sub>	4	4	Р	Negative power supply			
V <sub>S+</sub>	7	7	Р	Positive power supply			

(1) I= input, O = output, POW= power, and NC = no internal connection



# 7 Specifications

#### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)(1)

			MIN	MAX	UNIT
Vs	Supply voltage			33	V
VI	Input voltage	Input voltage		±V <sub>S</sub>	V
V <sub>ID</sub>	Differential input voltage			±4	V
Io	Output current	Output current		350	mA
		Maximum		150	
T <sub>J</sub> <sup>(2)</sup>	Junction temperature	Continuous operation, long-term reliability		125	°C
T <sub>stg</sub>	Storage temperature		-65	150	°C

- (1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) The maximum junction temperature for continuous operation is limited by package constraints. Operation above this temperature can result in reduced reliability, reduced lifetime of the device, or both.

#### 7.2 ESD Ratings

			VALUE	UNIT
V		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	\/
V <sub>(ESD)</sub>	Electrostatic discharge	Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	±1500	V

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

#### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

			MIN	NOM	MAX	UNIT
V <sub>S</sub>	Supply voltage Dual supply Single supply	Dual supply	±5	±15	±16	
		10	30	32	v	
T <sub>A</sub>	Operating free-air temperature		-40		85	°C

#### 7.4 Thermal Information

THERMAL METRIC(1)		THS309x	THS3091	
		DDA (SO PowerPAD)	DGN (HVSSOP)	UNIT
		8 PINS	8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	58.4	60.4	°C/W
R <sub>0JC(top)</sub>	Junction-to-case (top) thermal resistance	72.0	87.2	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	32.6	32.6	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	13.2	7.8	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	32.5	32.6	°C/W
R <sub>0JC(bot)</sub>	Junction-to-case (bottom) thermal resistance	17.1	17.0	°C/W

<sup>(1)</sup> For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.



# 7.5 Electrical Characteristics: $V_S = \pm 15 \text{ V}$

at  $T_A \cong 25^{\circ}C$ ,  $R_F = 1.21 \text{ k}\Omega$ ,  $R_L = 100 \Omega$ , and G = 2 (unless otherwise noted)

PARAMETER	TEST CON	IDITIONS	MIN	TYP	MAX	UNIT
AC PERFORMANCE						
	$G = 1$ , $R_F = 1.78$ kΩ,	DDA package		715		
	$V_O = 200 \text{ mV}_{PP}$	DGN package		600		
Small-signal bandwidth, –3 dB	$G = 2$ , $R_F = 1.21$ kΩ, $V_O =$	= 200 mV <sub>PP</sub>		305		MHz
	$G = 5$ , $R_F = 1 k\Omega$ , $V_O = 20$	00 mV <sub>PP</sub>		205		
	G = 10, R <sub>F</sub> = 866 Ω, V <sub>O</sub> =	200 mV <sub>PP</sub>		190		
0.1-dB bandwidth flatness	V <sub>O</sub> = 200 mV <sub>PP</sub>			95		MHz
Large-signal bandwidth	$G = 5, R_F = 1 k\Omega, V_O = 4$	V <sub>PP</sub>		135		MHz
Olympia (400) to 000/ lovel)	G = 2, V <sub>O</sub> = 10-V step, R <sub>F</sub>	= 1.21 kΩ		3600		\ //
Slew rate (10% to 90% level)	G = 5, V <sub>O</sub> = 20-V step, R <sub>F</sub>	= 1 kΩ		6000		V/µs
Rise and fall time	V <sub>O</sub> = 5 V <sub>PP</sub>			2		ns
		to 0.1%	-	12.5		
Settling time	$G = -2$ , $V_O = 2$ - $V_{PP}$ step	to 0.01%	,	18.5		ns
HARMONIC DISTORTION			,	,		
	.,	R <sub>L</sub> = 100Ω		72		dBc
2nd harmonic distortion	$V_O = 2 V_{PP}$ , $f = 10 MHz$	R <sub>L</sub> = 1 kΩ		84		
	V <sub>O</sub> = 2 V <sub>PP</sub> , f = 10 MHz	R <sub>L</sub> = 100 Ω	-	70		
3rd harmonic distortion		R <sub>L</sub> = 1 kΩ		99		dBc
Input voltage noise	f > 10 kHz		,	1.1		nV/√Hz
Noninverting input current noise	f > 10 kHz			15		pA/√Hz
Inverting input current noise	f > 10 kHz			14		pA/√Hz
DC PERFORMANCE		<u> </u>				
On an large francisco de la co	V .75V 0 4	T <sub>A</sub> = 25°C	350	1800		
Open-loop transimpedance	$V_0 = \pm 7.5 \text{ V, G} = 1$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	300			kΩ
land off about to	.,	T <sub>A</sub> = 25°C		0.9	3	
Input offset voltage	$V_{CM} = 0 V$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			5	mV
No. of the control of	.,	T <sub>A</sub> = 25°C		4	15	
Noninverting input bias current	V <sub>CM</sub> = 0 V	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			20	μA
In a section of the s	.,	T <sub>A</sub> = 25°C		3.5	15	
Inverting input bias current	$V_{CM} = 0 V$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			25	μA
lunch offer the comment	.,	T <sub>A</sub> = 25°C		1.7	20	
Input offset current	V <sub>CM</sub> = 0 V	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			30	μA
Average offset voltage drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$	+85°C		±19		μV/°C
Average noninverting bias current drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$	+85°C		±20		nA/°C
Average inverting bias current drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$	+85°C		±80		nA/°C
Average offset current drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$			±80		nA/°C



# 7.5 Electrical Characteristics: $V_S = \pm 15 V$ (continued)

at  $T_A \cong 25^{\circ}C$ ,  $R_F = 1.21 \text{ k}\Omega$ ,  $R_L = 100 \Omega$ , and G = 2 (unless otherwise noted)

PARAMETER	TEST CON	NDITIONS	MIN	TYP	MAX	UNIT
INPUT CHARACTERISTICS						
O	T <sub>A</sub> = 25°C		±13.3	±13.6		
Common-mode input range	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$		±13			V
Commence and a majoration matic	V = 140 V	T <sub>A</sub> = 25°C	62	78		٦D
Common-mode rejection ratio	V <sub>CM</sub> = ±10 V	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	59			dB
Noninverting input resistance				0.7		ΜΩ
Noninverting input capacitance				2.4		pF
Inverting input resistance				30		Ω
Inverting input capacitance				1.4		pF
OUTPUT CHARACTERISTICS						
	D 410	T <sub>A</sub> = 25°C	±12.8	±13.2		
Output voltage swing	$R_L = 1 k\Omega$	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$	±12.5	,		\ /
	D - 400 O	T <sub>A</sub> = 25°C	±12.1	±12.5		V
	R <sub>L</sub> = 100 Ω	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$	±11.8			
Output current	Sourcing D = 40.0	T <sub>A</sub> = 25°C	225	310		mA
	Sourcing, $R_L = 40 \Omega$	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$	200			
	Cinking D = 40.0	T <sub>A</sub> = 25°C	200	310		
	Sinking, $R_L = 40 \Omega$	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$	175	,		
Output impedance	f = 1 MHz, closed loop			0.06		Ω
POWER SUPPLY	'	,				
Ovice and assument	T <sub>A</sub> = 25°C	T <sub>A</sub> = 25°C		9.5	10.5	Л
Quiescent current	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	T <sub>A</sub> = -40°C to +85°C		,	11	mA
	. 0000	T <sub>A</sub> = 25°C	70	85		dB
Davis a sumply main ation	+PSRR	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	65			
Power supply rejection	-PSRR	T <sub>A</sub> = 25°C	68	82		
	-PSKK	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$	65			
POWER-DOWN CHARACTERISTIC	CS (THS3095 ONLY)			,	,	
REF voltage range <sup>((1))</sup>			V <sub>S-</sub>		$V_{S+}-4$	V
	Enable		Ī	PD ≥ REF		
Power-down voltage level <sup>(1)</sup>	Enable		+2			V
3	Disable		Ī	PD ≤ REF +0.8		
		T <sub>A</sub> = 25°C		500	700	
Power-down quiescent current	<u>PD</u> = 0 V	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$			800	μΑ
		T <sub>A</sub> = 25°C		11	15	
	$\overline{PD} = 0 \text{ V, REF} = 0 \text{ V,}$	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$		- 11	20	
PD bias current		T <sub>A</sub> = 25°C		11	15	μΑ
	PD = 3.3 V, REF = 0 V	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$			20	
Turn-on time delay	90% of final value	1.A 10 0 to 100 0		60	20	
Turn-off time delay	10% of final value			150		μs
rain on time delay	1070 Of fillal value			100		

<sup>(1)</sup> For detailed information on the behavior of the power-down circuit, see Section 8.3.1.



# 7.6 Electrical Characteristics: $V_S = \pm 5 V$

at  $T_A \cong 25^{\circ}\text{C}$ ,  $R_F = 1.15 \text{ k}\Omega$ ,  $R_L = 100 \Omega$ , and G = 2 (unless otherwise noted)

PARAMETER	TEST CON	DITIONS	MIN	TYP	MAX	UNIT
AC PERFORMANCE						
	$G = 1$ , $R_F = 1.78$ kΩ,	DDA package		485		
	$V_O = 200 \text{ mV}_{PP}$	DGN package	,	435		
Small-signal bandwidth, –3 dB	$G = 2$ , $R_F = 1.15$ kΩ, $V_O =$	200 mV <sub>PP</sub>	,	215		MHz
	$G = 5$ , $R_F = 1 k\Omega$ , $V_O = 20$	00 mV <sub>PP</sub>		160		
	G = 10, R <sub>F</sub> = 866 Ω, V <sub>O</sub> =	200 mV <sub>PP</sub>		160		
0.1-dB bandwidth flatness	V <sub>O</sub> = 200 mV <sub>PP</sub>			50		MHz
Large-signal bandwidth	V <sub>O</sub> = 4 V <sub>PP</sub>		,	205		MHz
Olemante (400), to 000), levelly	G = 2, V <sub>O</sub> = 5-V step, R <sub>F</sub> =	: 1.21 kΩ	,	1800		\ //
Slew rate (10% to 90% level)	G = 5, V <sub>O</sub> = 5-V step, R <sub>F</sub> =	: 1.21 kΩ		1700		V/µs
Rise and fall time	G = 2, V <sub>O</sub> = 5-V step, R <sub>F</sub>	= 1.21 kΩ		2		ns
Cattling times	0 - 0 1/ - 0 1/	to 0.1%		12.5		
Settling time	$G = -2$ , $V_O = 2$ - $V_{PP}$ step	to 0.01%	,	26		ns
HARMONIC DISTORTION					'	
and harmania distartion	V <sub>O</sub> = 2 V <sub>PP</sub> , f = 10 MHz	R <sub>L</sub> = 100 Ω		74		dD.
2nd harmonic distortion	V <sub>O</sub> = 2 V <sub>PP</sub> , I = 10 ΜΠΖ	R <sub>L</sub> = 1 kΩ		76		- dBc
2nd b distantis	V <sub>O</sub> = 2 V <sub>PP</sub> , f = 10 MHz	R <sub>L</sub> = 100 Ω		70		4D.
ord harmonic distortion		R <sub>L</sub> = 1 kΩ		75		dBc
Input voltage noise	f > 10 kHz			1.1		nV/√H:
Noninverting input current noise	f > 10 kHz			15		pA/√H:
Inverting input current noise	f > 10 kHz			14		pA/√H:
DC PERFORMANCE	'	1				
Onen leen transimusedense	V = 12.5 V C = 1	T <sub>A</sub> = 25°C	250	1500		10
Open-loop transimpedance	V <sub>O</sub> = ±2.5 V, G = 1	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	200			kΩ
Input offect valters	V -0V	T <sub>A</sub> = 25°C		0.6	2	m)/
Input offset voltage	V <sub>CM</sub> = 0 V	T <sub>A</sub> = -40°C to +85°C			3.5	mV
Namina antina in a state a summant	V - 0 V	T <sub>A</sub> = 25°C		2	15	
Noninverting input bias current	V <sub>CM</sub> = 0 V	T <sub>A</sub> = -40°C to +85°C			20	μA
Inverting input high current	V -0V	T <sub>A</sub> = 25°C		5	15	μΑ
Inverting input bias current	V <sub>CM</sub> = 0 V	T <sub>A</sub> = -40°C to +85°C			25	μA
Input offect current	V -0V	T <sub>A</sub> = 25°C		1.5	10	
Input offset current	$V_{CM} = 0 \text{ V}$ $T_{A} = -40^{\circ}\text{C to } +85^{\circ}\text{C}$			20	μA	
Average offset voltage drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$	+85°C		±20		μV/°C
Average noninverting bias current drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$	+85°C		±20		nA/°C
Average inverting bias current drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$	+85°C		±95		nA/°C
Average offset current drift	$V_{CM} = 0 \text{ V}, T_A = -40^{\circ}\text{C to}$	+85°C		±90		nA/°C



# 7.6 Electrical Characteristics: $V_S = \pm 5 V$ (continued)

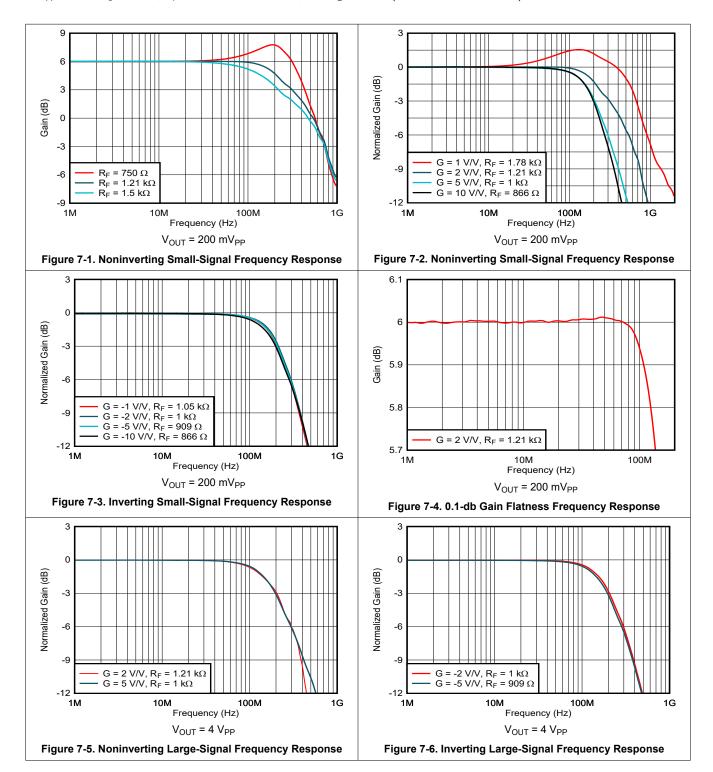
at  $T_A \cong 25^{\circ}C$ ,  $R_F = 1.15 \text{ k}\Omega$ ,  $R_L = 100 \Omega$ , and G = 2 (unless otherwise noted)

PARAMETER	TEST CON	NDITIONS	MIN	TYP	MAX	UNIT		
INPUT CHARACTERISTICS								
O	T <sub>A</sub> = 25°C		±3.3	±3.6				
Common-mode input range	T <sub>A</sub> = -40°C to +85°C		±3			V		
Common mode rejection ratio	$V_{CM} = \pm 2.0 \text{ V}, V_{O} = 0 \text{ V}$	T <sub>A</sub> = 25°C	60	66		40		
Common-mode rejection ratio	V <sub>CM</sub> - ±2.0 V, V <sub>O</sub> - 0 V	T <sub>A</sub> = -40°C to +85°C	57			dB		
Noninverting input resistance				0.45		МΩ		
Noninverting input capacitance				2.6		pF		
Inverting input resistance				32		Ω		
Inverting input capacitance				1.5		pF		
OUTPUT CHARACTERISTICS								
Output voltage owing	R <sub>L</sub> = 1 kΩ	T <sub>A</sub> = 25°C	±3.1	±3.4				
Output voltage swing	KL - 1 K22	T <sub>A</sub> = -40°C to +85°C	±2.8			V		
Output voltage eving	R <sub>L</sub> = 100 Ω	T <sub>A</sub> = 25°C	±2.7	±3.1		V		
Output voltage swing	11 - 100 12	$T_A = -40$ °C to +85°C	±2.5					
	Sourcing, R <sub>L</sub> = 10 Ω	T <sub>A</sub> = 25°C	140	250		mA		
Output current	Sourcing, NL = 10 12	$T_A = -40$ °C to +85°C	120					
Output current	Sinking, $R_L = 10 \Omega$	T <sub>A</sub> = 25°C	-140	-250		шА		
	Silikilig, INL - 10 12	$T_A = -40$ °C to +85°C	-120					
Output impedance	f = 1 MHz, closed loop			0.09		Ω		
POWER SUPPLY								
Quiescent current	T <sub>A</sub> = 25°C		7	8.2	9	mA		
Quiescent current	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$		6.5		9.5			
	+PSRR	T <sub>A</sub> = 25°C	68	81				
Power supply rejection	TFORK	$T_A = -40$ °C to +85°C	63			dB		
Tower supply rejection	-PSRR	T <sub>A</sub> = 25°C	65	79		αь		
	-i Sitit	T <sub>A</sub> = -40°C to +85°C	60					
POWER-DOWN CHARACTERISTIC	S (THS3095 ONLY)		·					
REF voltage range <sup>((1))</sup>			V <sub>S-</sub>		V <sub>S+</sub> – 4	V		
Davies davis valtaria laval(1)	Enable			PD ≥ REF+2				
Power-down voltage level <sup>(1)</sup>	Disable			PD ≤ REF+0.8		V		
Dower down guiest	DD = 0.1/	T <sub>A</sub> = 25°C		300	500	, . ^		
Power-down quiescent current	PD = 0 V	T <sub>A</sub> = -40°C to +85°C			600	μA		
	DD = 0.1/ DEC = 0.1/	T <sub>A</sub> = 25°C		11	15			
DD bigg gurrent	PD = 0 V, REF = 0 V,	T <sub>A</sub> -40°C to +85°C			20	, . ^		
PD bias current	DD - 222/ DEE - 22/	T <sub>A</sub> = 25°C		11	15	μA		
	PD = 3.3 V, REF = 0 V	T <sub>A</sub> = -40°C to +85°C			20			
		· A			- 1			
Turn-on time delay	90% of final value	TA TO THE COLUMN		60		μs		

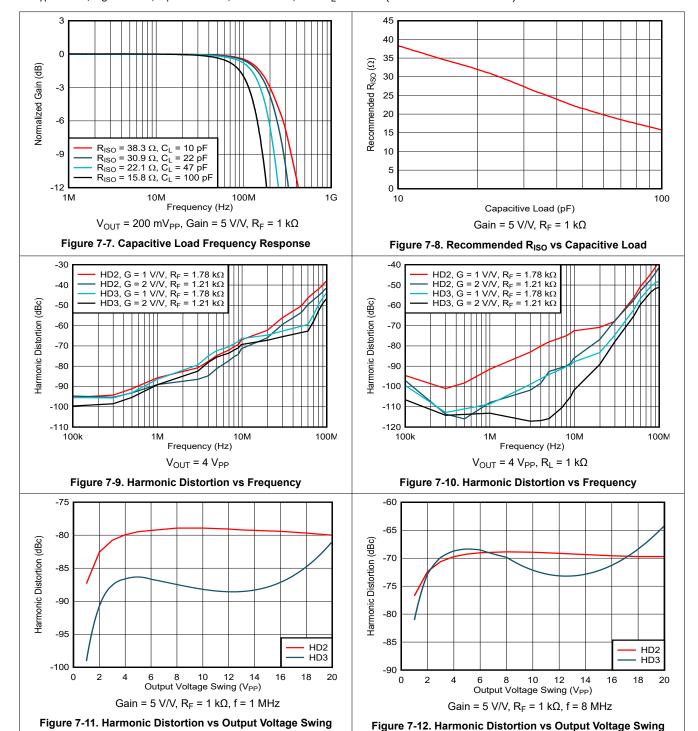
<sup>(1)</sup> For detailed information on the behavior of the power-down circuit, see Section 8.3.1.



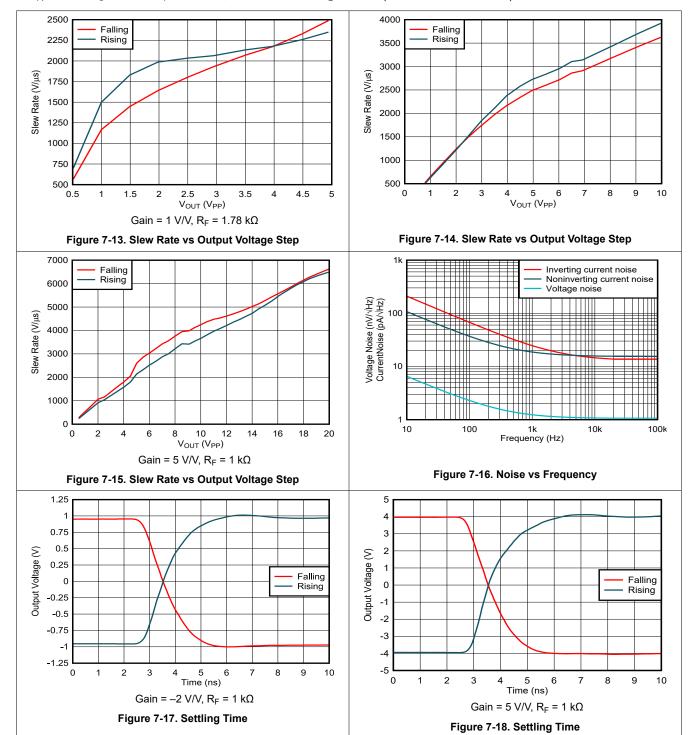
#### 7.7 Typical Characteristics: ±15 V





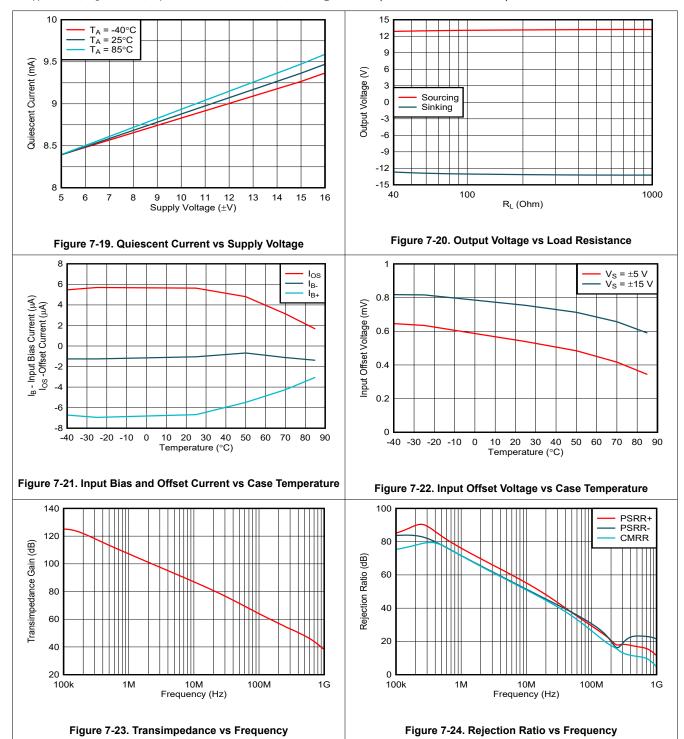




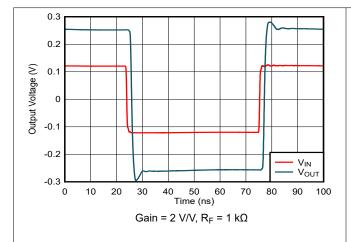




at T<sub>A</sub>  $\cong$  25°C, V<sub>S</sub> = ±15 V, R<sub>F</sub> = 1.21 k $\Omega$ , G = +2 V/V, and R<sub>L</sub> = 100  $\Omega$  (unless otherwise noted)







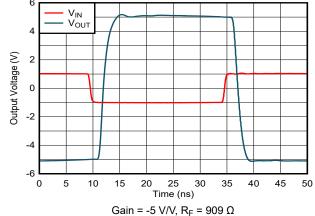
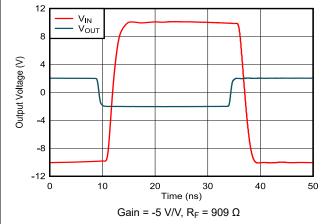


Figure 7-25. Noninverting Small-Signal Transient Response

Figure 7-26. Inverting Large-Signal Transient Response



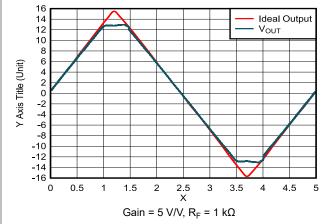
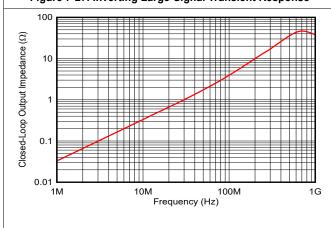


Figure 7-27. Inverting Large-Signal Transient Response

Figure 7-28. Output Overdrive Recovery Time



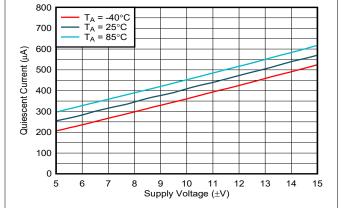
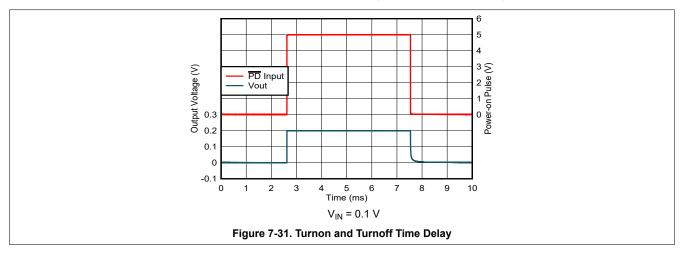


Figure 7-29. Closed-Loop Output Impedance vs Frequency

Figure 7-30. Power-Down Quiescent Current vs Supply Voltage

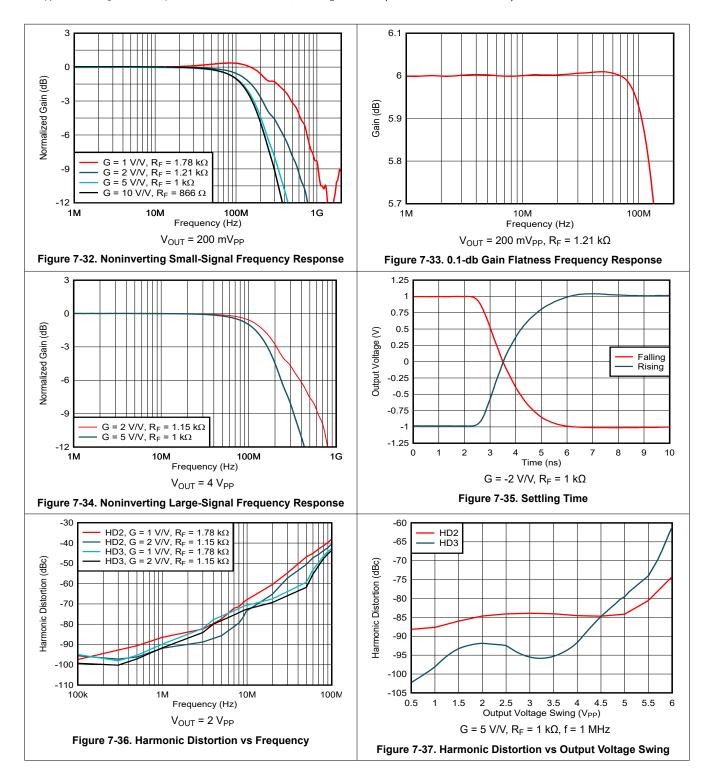


at T<sub>A</sub>  $\cong$  25°C, V<sub>S</sub> = ±15 V, R<sub>F</sub> = 1.21 k $\Omega$ , G = +2 V/V, and R<sub>L</sub> = 100  $\Omega$  (unless otherwise noted)

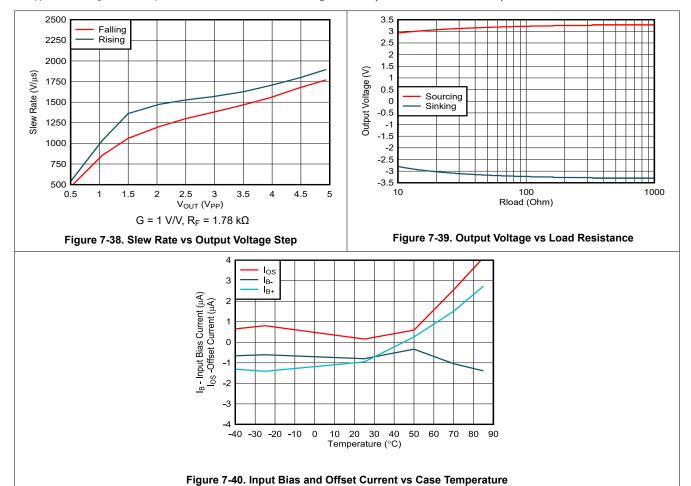




#### 7.8 Typical Characteristics: ±5 V







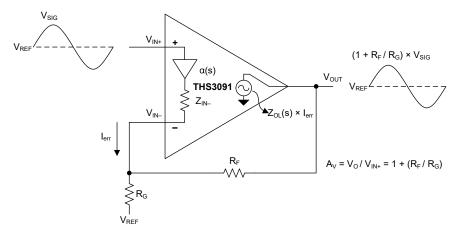
#### **8 Detailed Description**

#### 8.1 Overview

The THS3091 and THS3095 (THS309x) are high-voltage, low-distortion, high-speed, current feedback amplifiers. The THS309x are designed to operate over a wide supply range of ±5 V to ±16 V for applications requiring large, linear output swings, such as arbitrary waveform generators.

The THS3095 also features a power-down pin that puts the amplifier into a low-power standby mode, and lowers the quiescent current from 9.5 mA to  $500 \mu\text{A}$ .

#### 8.2 Functional Block Diagram



#### 8.3 Feature Description

#### 8.3.1 Power-Down and Reference Pins Functionality

The THS3095 features a power-down pin  $(\overline{PD})$  designed to reduce system power that lowers the quiescent current from 9.5 mA down to 500  $\mu$ A. The THS3095 also features a reference pin (REF) that allows the user to control the enable or disable power-down voltage levels applied to the  $\overline{PD}$  pin.

The power-down pin of the amplifier defaults to the positive supply voltage in the absence of an applied voltage, putting the amplifier in the power-on mode of operation. Driving the power-down pin towards the negative rail will turn off the amplifier and conserve power The following equations show the relationship between the reference voltage and the power-down thresholds:

$$\overline{PD} \le REF + 0.8 V \text{ for disable}$$
 (1)

$$\overline{PD} \le REF + 2.0 V for enable$$
 (2)

where the usable range at the REF pin is:

$$V_{S-} \leq V_{REF} \leq (V_{S+} - 4V) \tag{3}$$

The recommended mode of operation is to tie the REF pin to midrail, thus setting the disable or enable thresholds to the following equations:

$$V_{midrail} + 0.8 V$$
 (4)

$$V_{midrail} + 2V$$
 (5)

Power-Down mode is not intended to provide a high-impedance output. In other words, the power-down functionality is not intended to allow use as a tri-state bus driver. When in Power-Down mode, the impedance at the output of the amplifier is dominated by the feedback and gain-setting resistors, but the output impedance of the device varies depending on the voltage applied to the outputs.

Figure 8-1 shows the total system output impedance, which includes the amplifier output impedance in parallel with the feedback plus gain resistors, and cumulates to 2416  $\Omega$ . Figure 8-2 shows this circuit configuration for reference.

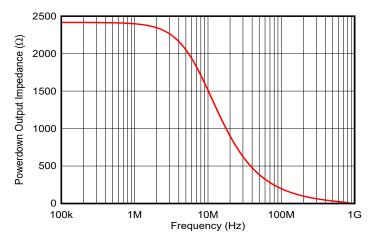


Figure 8-1. Power-Down Output Impedance vs Frequency

As with most current feedback amplifiers, the internal architecture places some limitations on the system when in Power-Down mode. Most notably is the fact that the amplifier actually turns on if there is a  $\pm 0.7$  V or greater difference between the two input nodes ( $V_{IN+}$  and  $V_{IN-}$ ) of the amplifier. If this difference exceeds  $\pm 0.7$  V, then the output of the amplifier creates an output voltage equal to approximately [( $V_{IN+} - V_{IN-}$ ) – 0.7 V] × Gain. This also implies that if a voltage is applied to the output while in Power-Down mode, the V– node voltage is equal to  $V_{O(applied)} \times R_G$  / ( $R_F + R_G$ ). For low-gain configurations and a large applied voltage at the output, the amplifier can actually turn on due to the aforementioned behavior.

The time delays associated with turning the device on and off are specified as the time required for the amplifier to reach either 10% or 90% of the final output voltage. The time delays are in the order of microseconds because the amplifier moves in and out of the linear mode of operation in these transitions.

#### 8.4 Device Functional Modes

#### 8.4.1 Wideband, Noninverting Operation

The THS309x are unity gain stable 715-MHz current-feedback operational amplifiers designed to operate from a  $\pm 5$ -V to  $\pm 15$ -V power supply. Figure 8-2 shows the THS3091 in a noninverting gain of 2-V/V configuration typically used to generate the performance curves. Most of the curves were characterized using signal sources with a 50- $\Omega$  source impedance, and with measurement equipment presenting a 50- $\Omega$  load impedance.

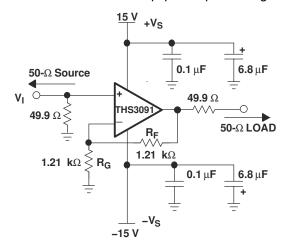


Figure 8-2. Wideband, Noninverting Gain Configuration

Current-feedback amplifiers are highly dependent on feedback resistor  $R_F$  for maximum performance and stability. Table 8-1 shows the optimal gain-setting resistors  $R_F$  and  $R_G$  at different gains to give maximum bandwidth with minimal peaking in the frequency response. Higher bandwidths can be achieved (at the expense of added peaking in the frequency response) by using even lower values for  $R_F$ . Conversely, increasing  $R_F$  decreases the bandwidth, but improves stability.

Table 8-1. Recommended Resistor Values for Optimum Frequency Response

THS30	THS3091 AND THS3095 $R_{F}$ AND $R_{G}$ VALUES FOR MINIMAL PEAKING WITH $R_{L}$ = 100 $\Omega$									
GAIN (V/V)	SUPPLY VOLTAGE (V)	R <sub>G</sub> (Ω)	R <sub>F</sub> (Ω)							
1	±5 and ±15	_	1.78 k							
2	±5	1.15 k	1.15 k							
2	±15	1.21 k	1.21 k							
5	±5 and ±15	249	1 k							
10	±5 and ±15	95.3	866							
-1	±5 and ±15	1.05 k	1.05 k							
-2	±5 and ±15	499	1 k							
<b>-</b> 5	±5 and ±15	182	909							
-10	±5 and ±15	86.6	866							



# 9 Application and Implementation

#### **Note**

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

#### 9.1 Application Information

#### 9.2 Typical Application

The fundamental concept of load sharing is to drive a load using two or more of the same operational amplifiers. Each amplifier is driven by the same source. Figure 9-1 illustrates the schematic for this design. This concept effectively reduces the current load of each amplifier by 1/N, where N is the number of amplifiers. For further details on the design and performance of this circuit, see the *Reference Design for Implementation of the Load Sharing Concept for Large-Signal Applications*.

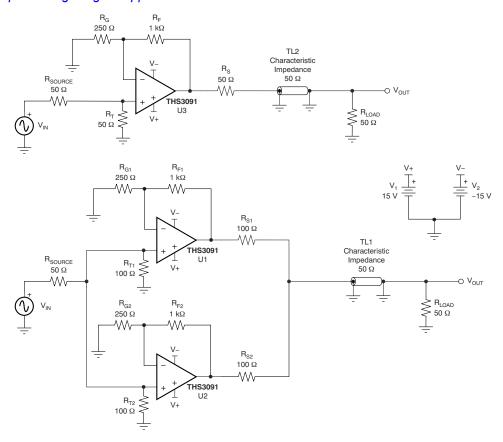


Figure 9-1. Reference THS3091 and THS3091 Load Sharing Test Configurations

#### 9.2.1 Design Requirements

Use two THS3091 amplifiers in a parallel load-sharing circuit to improve distortion performance.

Table 9-1. Design Parameters

140.00 1. 200.9 4.4								
DESIGN PARAMETER	VALUE							
V <sub>OPP</sub>	20 V							
R <sub>LOAD</sub>	100 Ω							

#### 9.2.2 Detailed Design Procedure

In addition to providing higher output current drive to the load, the load sharing configuration can also provide improved distortion performance. In many cases, an operational amplifier shows better distortion performance as the load current decreases (that is, for higher resistive loads) until the feedback resistor starts to dominate the current load. In a load sharing configuration of N amplifiers in parallel, the equivalent current load that each amplifier drives is 1/N times the total load current.

As shown in Figure 9-1 for example, in a two-amplifier load sharing configuration with matching resistance driving a resistive load (RL), each series resistance is 2×RL and each amplifier drives 2×RL. A convenient indicator of whether an op amp will function well in a load sharing configuration is the characteristic performance graph of harmonic distortion versus load resistance. Figure 7-9 and Figure 7-10 show more information. Such graphs can be found in most of Tl's high-speed amplifier data sheets. These graphs can be used to obtain a general sense of whether or not an amplifier will show improved distortion performance in load sharing configurations.

Figure 9-1 shows two test circuits: one for a single THS3091 amplifier driving a double-terminated (50- $\Omega$  cable), and one with two THS3091 amplifiers in a load sharing configuration. In the load sharing configuration, the two 100- $\Omega$  series output resistors act in parallel to provide 50- $\Omega$  back-matching to the 50- $\Omega$  cable.

Figure 9-2 and Figure 9-3 show the 32-MHz, 18-VPP sine wave output amplitudes for the single THS3091 configuration and the load sharing configuration, respectively, measured using an oscilloscope. An ideal sine wave is also included as a visual reference (the dashed red line). Figure 9-2 shows visible distortion in the single THS3091 output. In the load sharing configuration of Figure 9-3, however, no obvious degradation is visible.

Figure 9-4 and Figure 9-5 show the 64-MHz sine wave outputs of the two configurations from Figure 9-1. While the single THS3091 output is clearly distorted in Figure 9-4, the output of the load sharing configuration in Figure 9-5 shows only minor deviations from the ideal sine wave.

#### 9.2.3 Application Curves

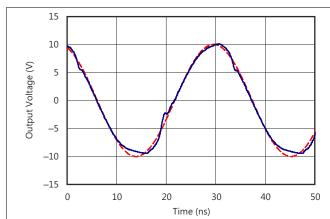


Figure 9-2. 32-MHz Sine Wave Output (Gain = 5 V/V, Signal Amplitude Referred to Amplifier Output), Single THS3091 Circuit Configuration

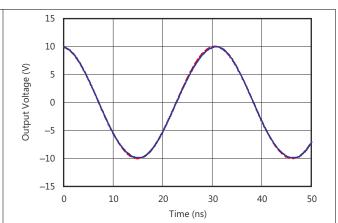


Figure 9-3. 32-MHz Sine Wave Output (Gain = 5 V/V, Signal Amplitude Referred to Amplifier Output), Two THS3091 Amplifiers in Load Sharing Configuration

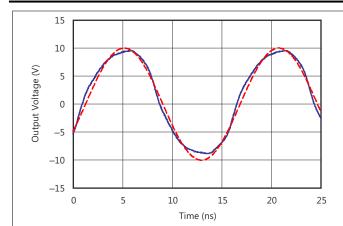


Figure 9-4. 64-MHz Sine Wave Output (Gain = 5 V/V, Signal Amplitude Referred to Amplifier Output), Single THS3091 Circuit Configuration

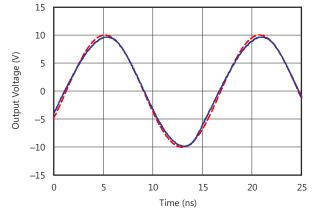


Figure 9-5. 64-MHz Sine Wave Output (Gain = 5 V/V, Signal Amplitude Referred to Amplifier Output), Two THS3091 Amplifiers in Load Sharing Configuration

#### 9.3 Power Supply Recommendations

The THS3091 operates using a single or dual supply as long as the input CM voltage range (CMIR) has the required headroom to either supply rail. Operating from a single supply has numerous advantages. With the negative supply at ground, the dc errors due to the –PSRR term are minimized. Decouple the supplies with low-inductance, ceramic capacitors to ground less than 0.5 inches from the device pins. The use of a ground plane is recommended; as in most high-speed devices, remove the ground plane near device sensitive pins such as the inputs. For split-supply operation, an optional supply decoupling capacitor across the two power supplies improves second harmonic distortion performance.



#### 9.4 Layout

#### 9.4.1 Layout Guidelines

To optimize performance with a high-frequency amplifier, such as the THS309x, pay careful attention to board layout parasitic and external component types.

Recommendations to optimize performance include the following:

- Minimize parasitic capacitance to any ac ground for all of the signal I/O pins. Parasitic capacitance on the
  output and input pins can cause instability. To reduce unwanted capacitance, open a window around the
  signal I/O pins in all of the ground and power planes around those pins. Otherwise, keep ground and power
  planes unbroken elsewhere on the board.
- Minimize the distance [< 0.25 inch (6.35 mm)] from the power supply pins to the high-frequency 0.1-μF and 100-pF decoupling capacitors. At the device pins, keep the ground and power plane layout away from the signal I/O pins. Avoid narrow power and ground traces to minimize inductance between the pins and the decoupling capacitors. Always decouple the power-supply connections with these capacitors. Use larger (6.8 μF or more) tantalum decoupling capacitors, effective at lower frequency, on the main supply pins. The decoupling capacitors can be placed somewhat farther from the device, and can be shared among several devices in the same area of the printed circuit board (PCB).</p>
- Connections to other wideband devices on the board can be made with short direct traces or through onboard transmission lines. For short connections, consider the trace and the input to the next device as a lumped capacitive load. Use relatively wide traces [0.05 inch (1.3 mm) to 0.1 inch (2.54 mm)], preferably with ground and power planes opened up around the traces. Estimate the total capacitive load and determine if isolation resistors on the outputs are necessary. Low-parasitic capacitive loads (< 4 pF) may not need an R<sub>ISO</sub> because the THS309x are nominally compensated to operate with a 2-pF parasitic load. Higher parasitic capacitive loads without an R<sub>ISO</sub> are allowed as the signal gain increases (increasing the unloaded phase margin).

#### 9.4.1.1 PowerPAD Design Considerations

The THS309x are available in a thermally-enhanced PowerPAD family of packages. These packages are constructed using a downset leadframe on which the die is mounted [see Figure 9-6(a) and Figure 9-6(b)]. This arrangement results in the lead frame being exposed as a thermal pad on the underside of the package [see Figure 9-6(c)]. Because this thermal pad has direct thermal contact with the die, excellent thermal performance can be achieved by providing a good thermal path away from the thermal pad. Note that devices such as the THS309x have no electrical connection between the PowerPAD and the die.

The PowerPAD package allows for both assembly and thermal management in one manufacturing operation. During the surface-mount solder operation (when the leads are being soldered), the thermal pad can also be soldered to a copper area underneath the package. Through the use of thermal paths within this copper area, heat can be conducted away from the package into either a ground plane or other heat-dissipating device.

The PowerPAD package represents a breakthrough in combining the small area and ease of assembly of surface mount with the awkward mechanical methods of heatsinking.

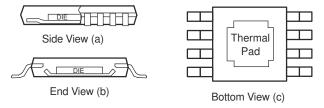


Figure 9-6. Views of Thermal Enhanced Package

Although there are many ways to properly heatsink the PowerPAD package, the following section lists the recommended steps.

#### 9.4.1.1.1 PowerPAD Layout Considerations

- 1. Figure 9-7 shows a PCB with a top-side etch pattern. Place an etch for the leads as well as etch for the thermal pad.
- 2. Place 13 holes in the area of the thermal pad. The recommended holes size is 0.01 inch (0.254 mm) in diameter. Keep the holes small so that solder wicking through the holes is not a problem during reflow.
- 3. Additional vias can be placed anywhere along the thermal plane outside of the thermal pad area. These additional vias help dissipate the heat generated by the THS309x device. The additional vias can be larger than the 0.01-inch (0.254 mm) diameter vias directly under the thermal pad. The additional vias can be larger because these vias are not in the thermal pad area to be soldered so that wicking is not a problem.
- 4. Connect all holes to the internal ground plane. The PowerPAD is electrically isolated from the silicon and all leads. Therefore, connecting the PowerPAD to any potential voltage, such as V<sub>S</sub>, is acceptable because there is no electrical connection to the silicon.
- 5. When connecting these holes to the ground plane, do not use the typical web or spoke via connection methodology. Web connections have a high thermal resistance that is useful for slowing the heat transfer during soldering operations. This high thermal resistance makes the soldering of vias that have plane connections easier. In this application, however, low thermal resistance is desired for the most efficient heat transfer. Therefore, connect the holes under the THS309x PowerPAD package connection to the internal ground plane with a complete connection around the entire circumference of the plated-through hole.
- 6. On the top-side solder mask, leave the terminals of the package and the thermal pad area with the 13 holes exposed. On the bottom-side solder mask, cover the 13 holes of the thermal pad area. This guideline prevents solder from being pulled away from the thermal pad area during the reflow process.
- 7. Apply solder paste to the exposed thermal pad area and all of the device pins.
- 8. With these preparatory steps in place, the device is simply placed in position and run through the solder reflow operation as with any standard surface-mount component. This process results in a device that is properly installed.

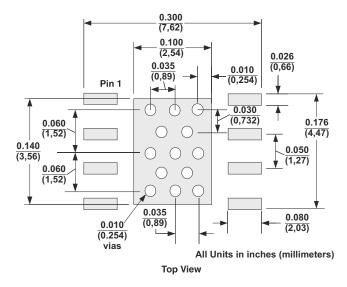


Figure 9-7. DDA PowerPAD PCB Etch and Via Pattern

#### 9.4.1.2 Power Dissipation and Thermal Considerations

The THS309x incorporates automatic thermal shutoff protection. This protection circuitry shuts down the amplifier if the junction temperature exceeds approximately 160°C. When the junction temperature reduces to approximately 140°C, the amplifier turns on again. But, for maximum performance and reliability, the designer must ensure that the design does not exceed a junction temperature of 125°C. Between 125°C and 150°C, damage does not occur, but the performance of the amplifier begins to degrade and long-term reliability suffers. The thermal characteristics of the device are dictated by the package and the PCB. Maximum power dissipation for a given package is calculated using the following equation:

$$P_{Dmax} = \frac{T_{max} - T_A}{\theta_{JA}} \tag{6}$$

#### Where:

- P<sub>Dmax</sub> is the maximum power dissipation in the amplifier (W).
- T<sub>max</sub> is the absolute maximum junction temperature (°C)
- T<sub>A</sub> is the ambient temperature (°C)
- $\theta_{JA} = \theta_{JC} + \theta_{CA}$
- θ<sub>JC</sub> is the thermal coefficient from the silicon junctions to the case (°C/W)
- θ<sub>CA</sub> is the thermal coefficient from the case to ambient air (°C/W)

For systems where heat dissipation is more critical, the THS3091 and THS3095 are offered in an 8-pin SOIC (DDA) with PowerPAD package. The thermal coefficient for the PowerPAD packages are substantially improved over the traditional SOIC. The data for the PowerPAD packages assume a board layout that follows the PowerPAD layout guidelines referenced above and detailed in the *PowerPAD<sup>TM</sup> Thermally Enhanced Package* application note. If the PowerPAD is not soldered to the PCB, then the thermal impedance increases substantially, which can cause serious heat and performance issues. Be sure to always solder the PowerPAD to the PCB to optimize performance.

When determining whether or not the device satisfies the maximum power-dissipation requirement, consider not only quiescent power dissipation, but also dynamic power dissipation. Often times, ynamic power dissipation is difficult to quantify because the signal pattern is inconsistent, but an estimate of the RMS power dissipation can provide visibility into a possible problem.



#### 9.4.2 Layout Example

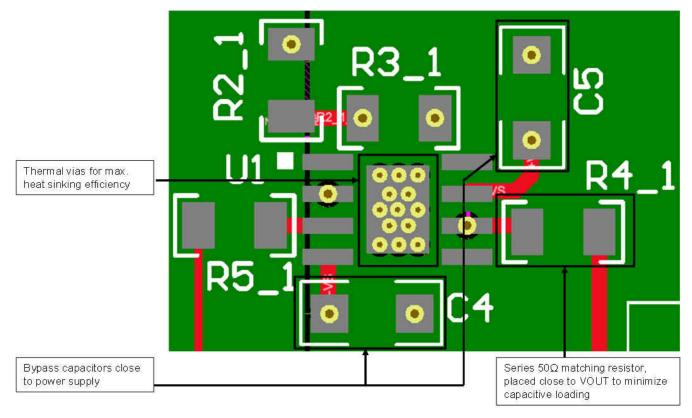


Figure 9-8. Layout Recommendation

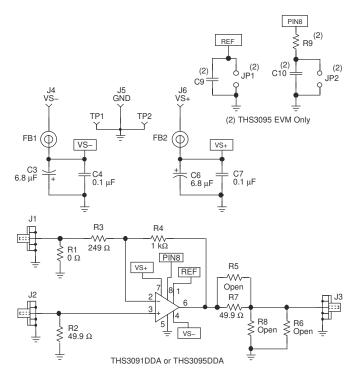
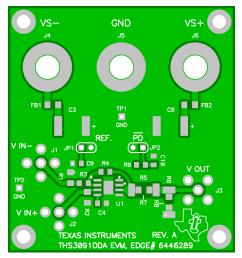
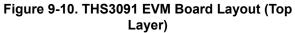


Figure 9-9. THS3091 EVM Circuit Configuration







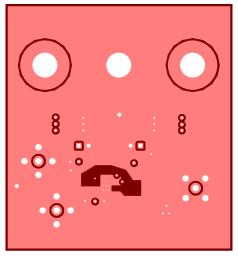


Figure 9-11. THS3091 EVM Board Layout (Second and Third Layers)

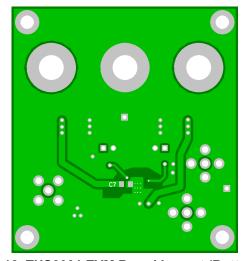


Figure 9-12. THS3091 EVM Board Layout (Bottom Layer)



# 10 Device and Documentation Support

### 10.1 Device Support

#### 10.1.1 Development Support

- TIDA-00684: High-Bandwidth Arbitrary Waveform Generator Reference Design: DC or AC coupled, High-Voltage output
- TIDA-00075: Wide-Bandwidth and High-Voltage Arbitrary Waveform Generator Front End
- TIDA-00023: Reference Design for Implementation of the Load Sharing Concept for Large-Signal Applications

#### **10.2 Documentation Support**

#### 10.2.1 Related Documentation

For related documentation, see the following:

- Texas Instruments, PowerPAD™ Made Easy application brief
- Texas Instruments, PowerPAD™ Thermally Enhanced Package technical brief
- Texas Instruments, Voltage Feedback vs Current Feedback Amplifiers application note
- Texas Instruments, Current Feedback Analysis and Compensation application note
- Texas Instruments, Current Feedback Amplifiers: Review, Stability, and Application application note
- Texas Instruments, Effect of Parasitic Capacitance in Op Amp Circuits application note
- Texas Instruments, Expanding the Usability of Current-Feedback Amplifiers analog journal

#### 10.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

#### 10.4 Support Resources

TI E2E™ support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

#### 10.5 Trademarks

PowerPAD™ and TI E2E™ are trademarks of Texas Instruments.

All trademarks are the property of their respective owners.

#### 10.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### 10.7 Glossary

TI Glossary This glossary lists and explains terms, acronyms, and definitions.

#### 11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead finish/ Ball material	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
THS3091D	LIFEBUY	SOIC	D	8	75	RoHS & Green	(6) NIPDAU	Level-1-260C-UNLIM	-40 to 85	3091	
THS3091DDA	ACTIVE	SO PowerPAD	DDA	8	75	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 85	3091	Samples
THS3091DDAG3	ACTIVE	SO PowerPAD	DDA	8	75	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 85	3091	Samples
THS3091DDAR	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 85	3091	Samples
THS3091DDARG3	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 85	3091	Samples
THS3091DR	LIFEBUY	SOIC	D	8	2500	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 85	3091	
THS3091IDGNR	ACTIVE	HVSSOP	DGN	8	2500	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	3091	Samples
THS3095D	LIFEBUY	SOIC	D	8	75	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 85	3095	
THS3095DDA	ACTIVE	SO PowerPAD	DDA	8	75	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 85	3095	Samples
THS3095DDAR	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 85	3095	Samples
XTHS3091IDGNR	ACTIVE	HVSSOP	DGN	8	2500	TBD	Call TI	Call TI	-40 to 85		Samples

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

<sup>(3)</sup> MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.



# **PACKAGE OPTION ADDENDUM**

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(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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#### TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
THS3091DDAR	SO PowerPAD	DDA	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
THS3091DR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
THS3091IDGNR	HVSSOP	DGN	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
THS3095DDAR	SO PowerPAD	DDA	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1



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#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
THS3091DDAR	SO PowerPAD	DDA	8	2500	350.0	350.0	43.0
THS3091DR	SOIC	D	8	2500	350.0	350.0	43.0
THS3091IDGNR	HVSSOP	DGN	8	2500	356.0	356.0	35.0
THS3095DDAR	SO PowerPAD	DDA	8	2500	350.0	350.0	43.0

# **PACKAGE MATERIALS INFORMATION**

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#### **TUBE**



\*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
THS3091D	D	SOIC	8	75	505.46	6.76	3810	4
THS3091DDA	DDA	HSOIC	8	75	505.46	6.76	3810	4
THS3091DDAG3	DDA	HSOIC	8	75	505.46	6.76	3810	4
THS3095D	D	SOIC	8	75	505.46	6.76	3810	4
THS3095DDA	DDA	HSOIC	8	75	505.46	6.76	3810	4

3 x 3, 0.65 mm pitch

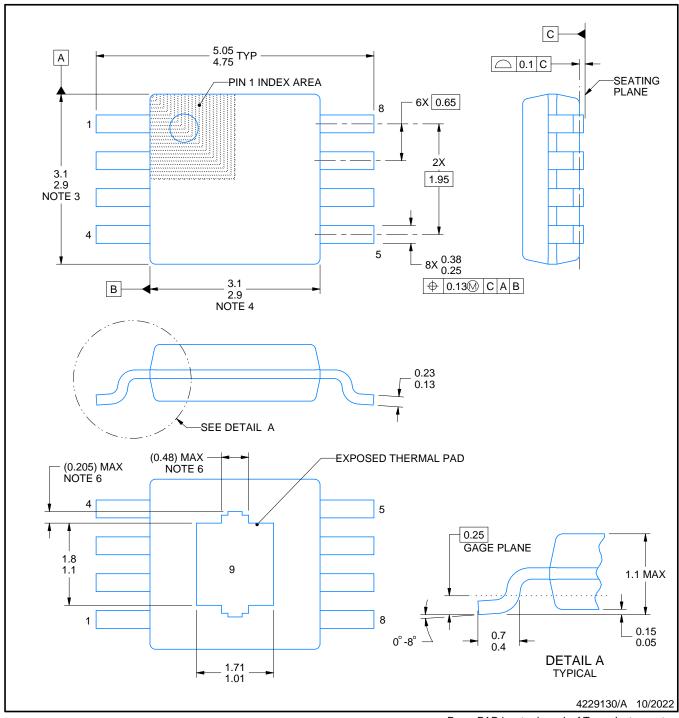
SMALL OUTLINE PACKAGE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



# PowerPAD<sup>™</sup> VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



#### NOTES:

PowerPAD is a trademark of Texas Instruments.

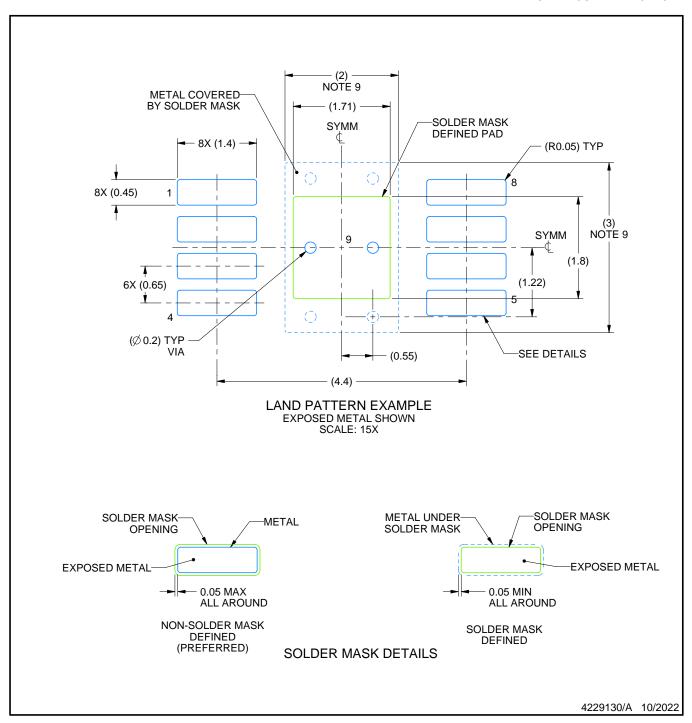
- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.
- 6. Features may differ or may not be present.



SMALL OUTLINE PACKAGE

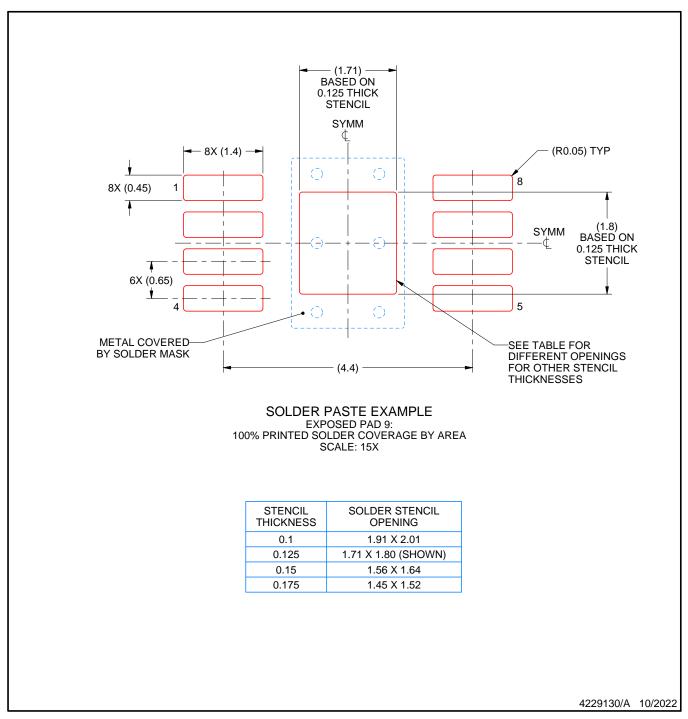


NOTES: (continued)

- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 9. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
- 10. Size of metal pad may vary due to creepage requirement.



SMALL OUTLINE PACKAGE



NOTES: (continued)

- 11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 12. Board assembly site may have different recommendations for stencil design.





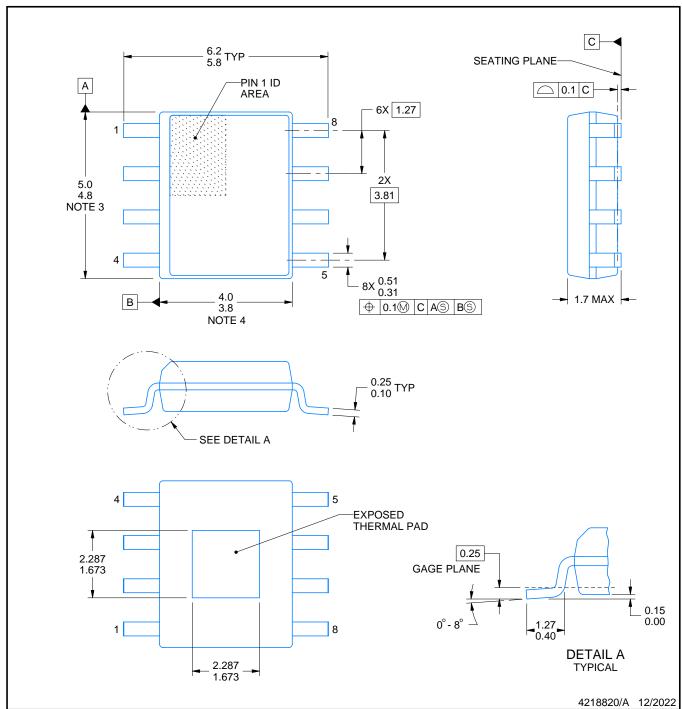
Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

4202561/G





PLASTIC SMALL OUTLINE



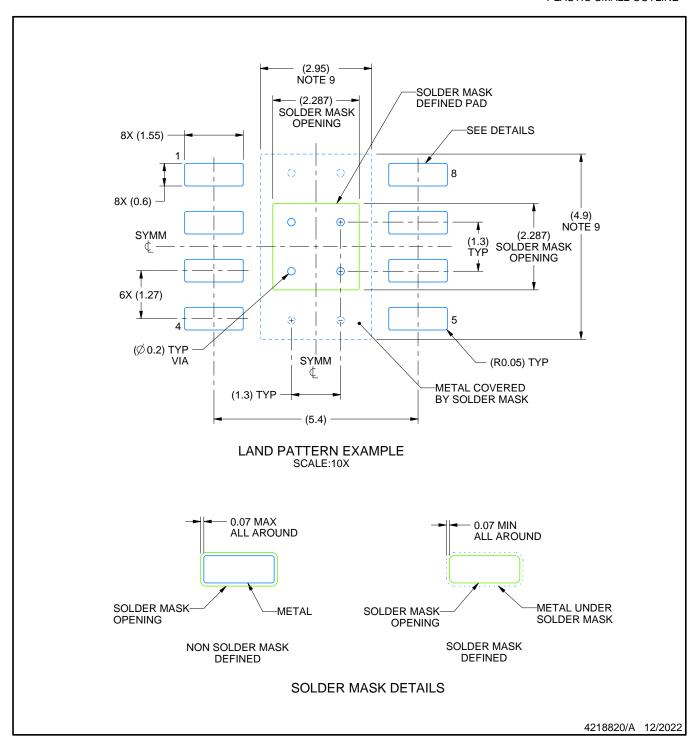
#### PowerPAD is a trademark of Texas Instruments.

#### NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MS-012, variation BA.



PLASTIC SMALL OUTLINE

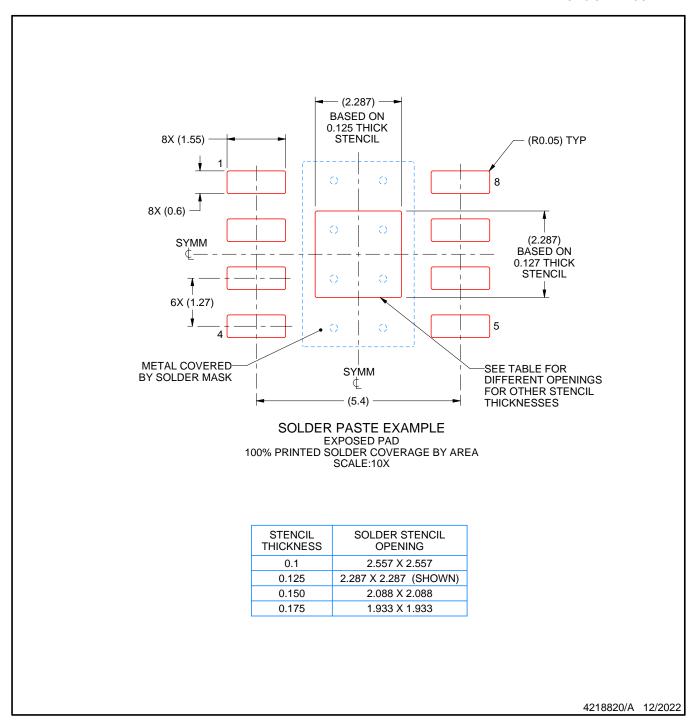


#### NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- Solder mask tolerances between and around signal pads can vary based on board fabrication site.
   This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Size of metal pad may vary due to creepage requirement.



PLASTIC SMALL OUTLINE



NOTES: (continued)

- 10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 11. Board assembly site may have different recommendations for stencil design.





SMALL OUTLINE INTEGRATED CIRCUIT



#### NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



#### NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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